

## CO-EVAPORATION OF CO-CR AT INTERMEDIATE OBLIQUE INCIDENCE

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## ABSTRACT

The co-evaporation technique has been used for deposition of Co-Cr layers. Deposition has been done under intermediate angle of incidence of opposing vapour streams. The layers showed a single phase hcp poly-crystalline structure. The (002) plane turned out to be tilted towards the direction of the Co source. The layers showed good perpendicular magnetic behaviour although the magnetic anisotropy axis was also inclined towards the Co-source. Because of the opposing angle of incidence for Co and Cr atoms, a process-induced segregation takes place which causes a relative high coercivity also at low process temperatures. A simple model for the segregation effect can explain the relation between the existence of a non-magnetic region and an increased coercivity of the Co-Cr film.

## INTRODUCTION

Co-Cr films are most promising as a perpendicular magnetic recording medium.  $D_{50}$  values of over 250 kBPI have been reported.[1]. Initially the layers were produced by r.f.sputtering[2] but later on various other methods have been used. In recent years the emphasis has been shifted towards high-rate techniques like magnetron sputtering [3] and vacuum evaporation[4]. The latter is the most promising from the point of view of deposition rate. This technology could provide a production process that could be competitive to the present particulate tape production[5].

The most intensive work on evaporated Co-Cr layers has been done by Sugita et.al.[4,6] who have researched the continuous deposition process. They have also studied angle of incidence effects and found that for a relatively small angle ( $\alpha_i < 30^\circ$ ;  $\alpha_i =$  deviation from normal incidence) no deterioration of the crystal structure could be observed. Others [7,8] have reported on the highly orientated Co-Cr layers, deposited on  $\alpha$ -Ge or Ti seedlayers which show a good recording performance. These results show that a high quality medium prepared by evaporation can be obtained.

In most of the published work on evaporation of Co-Cr an alloy source is applied. This results in problems with composition control caused by exhaustion of the Cr in the source[9]. An alternative for this method is the dual source evaporation technology. In this method a geometrical problem arises which could introduce a composition gradient along the layer thickness. This can be accepted because a continuous composition gradient can offer some merits[10].

In this paper results are shown from experiments, using the co-evaporation technique. Especially the properties that might arise from the not ideal situation of intermediate oblique incidence are discussed.

## EXPERIMENTAL SETUP

The deposition is carried out using a Leybold Heraeus L560 high vacuum system equipped with 2 e-beam evaporation sources. The individual deposition rate of the sources is controlled by two quartz-crystal thickness monitors. The geometry of the sources and substrate is shown in fig.1. During deposition, the substrate position is fixed. The angle of incidence to the substrate is  $21^\circ$ - $31^\circ$  (depending on the position on the substrate holder) and the Co and Cr atoms arrive from opposite directions. During deposition, the end pressure is at a level of  $P_e < 10^{-8}$  mbar, also at higher process temperatures. The deposition rate was 8 Å/s.

Single crystal Si wafers were used as substrate material. The substrates were tightly mounted against a substrate plate which is heated from the backside by an infra-red heater. The monitored process temperature ( $T_p$ ) is not the actual substrate temperature ( $T_{sub}$ ) but the control temperature of the infra-red heater.  $T_p$  is expected to be proportionally smaller than the actual  $T_{sub}$  and was in the range 50-300°C.

From every deposition cycle, several samples were analysed, each from a different position on the substrate holder and thus showing a change in their composition and slightly in their thickness.

The magnetic properties were measured by V.S.M and a torque magnetometer. The structure of the layers was analysed by X-ray diffraction (Co-K $\alpha$ ) and the so called rocking curve was measured. TEM analysis was performed in order to determine crystallinity and grain size.

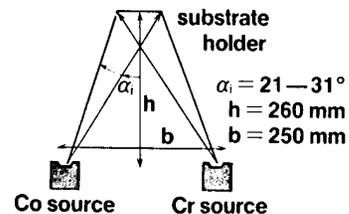


Fig. 1 Basic geometry of the process

## RESULTS AND DISCUSSION

## Structural analysis

Our first concern is if a proper crystallographic structure has been obtained. The TEM bright and dark field images and diffraction pattern indicated a polycrystalline texture with an average grain size of 10-15 nm for layer thickness  $\delta = 80$  nm. The samples with lower Cr content showed the largest grain size. The samples were also analysed by X-ray diffraction and only a (002) diffraction peak at  $2\theta = 52.4^\circ$  could be observed, indicating that only a hcp structure, perpendicularly orientated towards the substrate is formed in the layer. From this peak the so called rocking curve was measured. The half-value width  $\Delta\theta_{50}$  of the rocking curve peak, was 12-14° for  $\delta > 200$  nm. This is a relatively high value for Co-Cr layers; however, because of the oblique incidence this could be expected. Improved geometry and application of seedlayers will improve this orientation.

The rocking curve was measured for several rotation axes of the samples. The longitudinal (LP) and transversal (TP) measurement plane are defined in Fig.2.

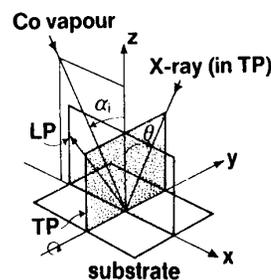


Fig. 2a  
Definition of the measurement planes

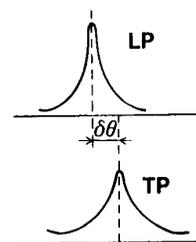


Fig. 2b  
Shift of peak in rocking curve

It was found that in the LP, the peak of the rocking curve was shifted over an angle  $\delta\theta$  from the peak that occurred in the TP. Also a lower peak value was measured in the TP. This shift in the longitudinal plane is caused by a preferential inclination of the [001] crystal axis towards the Co-source. The shift angle at  $\delta=400\text{nm}$  is  $\delta\theta=9-11^\circ$ , independent of the angle of incidence but seems to depend on the layer thickness ( $\delta\theta=5-7^\circ$  for  $\delta<200\text{nm}$ ).

Because of the oblique incidence, we might expect a canting  $\beta$  of the columns from the perpendicular direction according to [11]:

$$\beta = \arctan(0.5 \tan \alpha_1) \quad (1)$$

In our case the canting will be towards the direction of the Co source because most of the material in the layer is Co. Generally  $\beta$  is larger than the observed shift in the rocking curve. Unfortunately we have not yet performed an observation of the cross-sectional view by SEM in order to observe the actual angle of canting of the columns. However, on the basis of other experiments, we can obtain information on this canting. This will be discussed in combination with the results of our torque measurements.

Concerning the material properties of the layers, we can summarize a polycrystalline single-phase hcp structure with an orientation which is preferentially inclined through a number of degrees towards the direction of the incidence of the Co atoms.

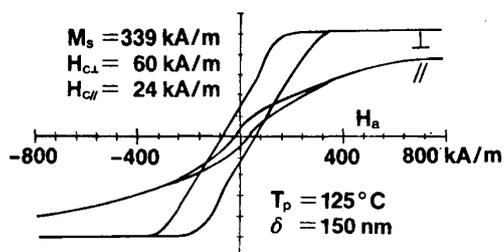


Fig. 3 Typical M-H loop of the Co-Cr layers

#### Magnetic properties

In Fig. 3, a typical M-H loop of the deposited layers is shown. A good perpendicular magnetic behaviour is obtained. The inplane coercivity ( $H_{c||}$ ) of the layers is 25-35 kA/m. Fig. 4 shows the perpendicular coercivity ( $H_{c\perp}$ ) versus saturation magnetization ( $M_s$ ). The thickness of these samples is near 200nm and deposition was carried out at several values of  $T_p$ . At constant  $M_s$ , a higher  $H_{c\perp}$  is observed for increasing  $T_p$ , as is usually found for Co-Cr layers. A comparison is shown of  $H_{c\perp}$  values of Ouchi[12] for 1  $\mu\text{m}$  sputter-deposited layers at  $T_{\text{sub}}=200^\circ\text{C}$  and those estimated from data of Sugita[4] for 0.15  $\mu\text{m}$  evaporated at  $T_{\text{sub}}=160^\circ\text{C}$ . It can be seen that a clear difference between the two methods exists in the high  $M_s$  region. In the former a maximum is found near  $M_s=700$  kA/m while in the latter this maximum occurs at lower  $M_s$  values. This will be due to the difference in energy of the vaporized atoms which is much higher in sputtering. Increasing  $T_p$  might partially compensate for the lower energy level at evaporation. However, for our co-evaporated samples, already at low  $T_p=50^\circ\text{C}$ , an increased  $H_{c\perp}$  is observed. A correlation between this result and the existence of a "Cr-rich" part in the Co-Cr layer can be found if we observe the relation between  $M_s$  and the mean Cr concentration ( $C_m$ ) as was measured by XRF. (see fig. 5). At higher Cr contents, a deviation from the bulk  $M_s$  value is measured. This deviation is more pronounced at higher  $T_p$ . Already at  $T_p=50^\circ\text{C}$  a considerable volume of "Cr-rich" Co-Cr must exist. This cannot only be due to a segregation by ad-atom diffusion during film growth. Therefore a process-induced segregation must also exist. This will be caused by shadowing effects

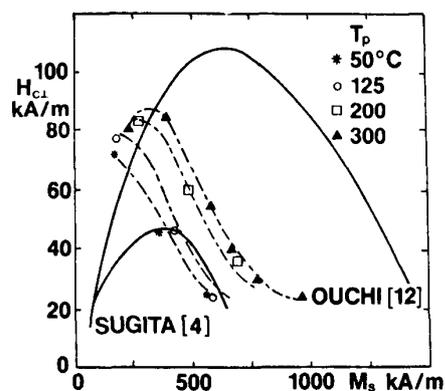


Fig. 4 Relation between  $H_{c\perp}$  and  $M_s$  of Co-Cr layers.

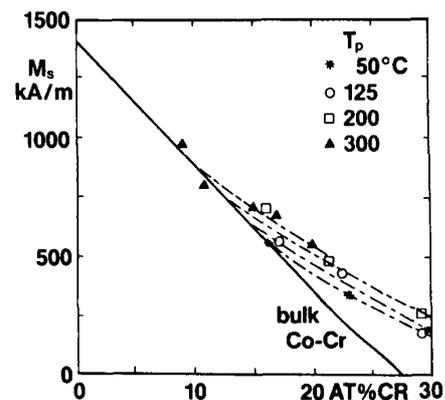


Fig. 5 Relation between  $M_s$  and the mean concentration.

during deposition under the opposing intermediate oblique incidence. A good treatment of such type of problem can be found in [13] showing these effects to occur in Fe-Cu layers deposited at varying angles of incidence.

The relation between the existence of this segregated state and the occurrence of an increased coercivity of the Co-Cr layers could be explained by a model introduced by Andr  and Danan[14]. This model is based on a grain boundary with increased Cr content which forms pinning points for domain-wall motion at low peak concentration and a non-magnetic boundary resulting in particulate behaviour at peak concentrations higher than 25-27 at% Cr.

We tried to fit the model, using (2) for the Cr distribution in a column, to our measured relation between  $C_m$  and  $M_s$ .

$$C(d) = C_c + (C_p - C_c) \cdot e^{-(D-d)^2/2W^2} \quad (0 < d < D) \quad (2)$$

with:

$C_c$  = column centre Cr concentration,  $C_p$  = Cr concentration at column boundary,  $D$  = column diameter  $W$  = measure for the column boundary width.

We modified the model to a better fit to the results of Sugita[6]. We assume  $C_p$  to depend only on  $C_c$  and a constant  $S_g$ , denoting the degree of segregation. Further we assume  $W/D$  to be constant for a certain  $C_c$ , independent of the degree of segregation. This can be understood from the fact that at higher  $T_p$  generally both segregation (and thus  $W$ ) but also the column size  $D$  increase. We assume  $W$  to be proportional to the potential amount of Cr that can segregate;  $C_c \cdot D$ . Thus:

$$C_p = S_g \cdot C_c \quad (3) \quad \text{and} \quad W/D = W_0/D \cdot C_c \quad (4)$$

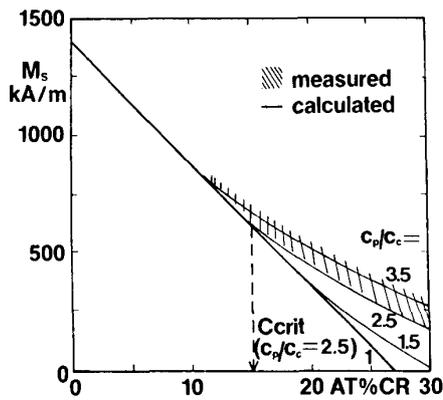


Fig. 6 Comparison between measured and calculated relation between  $M_s$  and  $C_m$ .

The fitting parameter  $W_o/D = 0.005$  will give a good fit with Sugita's results. We only have to change the relative peak concentration in this simple model in order to fit it to our  $M_s(C_m)$  curve. A reasonable agreement is obtained at  $C_p = 2.5-3.5 \cdot C_c$  as is shown in Fig. 6. It is clear in this figure that a significant deviation from the line of homogeneous distribution of Cr starts at a value  $C_m = C_{crit}$  which depends on the point when the peak concentration exceeds 27 at%Cr and thus a non-magnetic boundary is introduced. In most of the cases  $C_{crit}$  is near 15at% Cr. However, also at  $C_m < C_{crit}$  the segregation might exist but will not lead to an easily observable deviation from the line for bulk saturation magnetisation.

In other words,  $C_{crit}$  will indicate the start of the formation of the non-magnetic boundary and thus also the change in the reversal mechanism from domain-wall pinning into particulate behaviour. In our case,  $C_{crit} = 12-17at\%$  which is also near the point where an increased Hci is observed (fig. 4) as could be expected from a more particulate behaviour.

#### Magnetic anisotropy

In magnetic layers, deposited under oblique incidence, a magnetic anisotropy axis is found which is rotated towards the tilted columns [15]. Although our layers showed a typical magnetic behaviour of a layer with a perpendicularly orientated magnetic anisotropy, an inclined magnetic anisotropy exists. This could be detected by the torque magnetometer and using the method of Swaving *et al.* [16] to calculate the anisotropy constant and the direction of the anisotropy axis. For samples with  $\delta > 200nm$  we found a  $K_1 > 15 \cdot 10^4 J/m^3$ . (With  $K_1 = K_u - 1/2 \mu_0 M_s^2$ ) The angle of the anisotropy axis towards the film normal ( $\gamma_a$ ) depends on the angle of incidence  $\alpha_1$  on the sample. In table I the results are given together with the values of the other important directions which have been found. These samples were deposited at  $T_p = 125^\circ C$  and  $\delta = 400 nm$ .

Table I Relation between angle of incidence and other relevant angles for several material properties.

substrate position	$\alpha_1$	$\beta$	$\delta\theta$	$\gamma_a$
I	21°	11°	9-11°	9°
II	26°	14°	9-11°	14.5°
III	31°	17°	9-11°	16°

It can be seen that the anisotropy direction more or less coincides with the expected column canting. This would imply a significant contribution of shape anisotropy to the magnetic anisotropy. However, the appearance of the shift in the rocking curve also indicates a small rotation of the crystal axis towards

the column direction and thus the magnetic crystal anisotropy will also be rotated although this will not completely explain the full rotation of the magnetic anisotropy axis. We planned to further investigate this.

#### CONCLUSION

The deposition by co-evaporation under intermediate oblique incidence and opposing vapour streams has some significant influences on the properties of Co-Cr layers. In our investigations we found, besides the usually found properties, some process induced effects:

- a preferential inclined orientation of the single phase hcp structure towards the canted column.
- a rotation of the magnetic anisotropy axis to the canted column.

Both effects might be related to each other but the rotation of the crystal axis will not fully explain the rotation of the magnetic anisotropy axis. This might indicate that a shape anisotropy term will also occur. Notwithstanding this inclined anisotropy, the layers showed good perpendicular behaviour with high anisotropy energy. Based on the magnetic measurements we found:

- that at relative low process temperature we could obtain a high Hci (upto 70 kA/m) in the  $M_s$  range 200-500 kA/m.

This is due to a process-induced segregation caused by shadowing during deposition.

- By fitting a simple model for the Cr distribution to the measured  $M_s(C_m)$  curve, a  $C_{crit}$  can be defined at which point a non-magnetic boundary between magnetic Co-Cr parts is formed. This  $C_{crit}$  correlates with the increase of Hci vs  $M_s$  thus indicating the relation between the occurrence of this non-magnetic boundary and a particulate like behaviour of the magnetic reversal mechanism.

In general, these layers deposited under intermediate oblique incidence showed good perpendicular magnetic properties which might be improved by optimized geometrical design.

#### ACKNOWLEDGEMENT

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