

# Micro-bubbles and Micro-particles are Not Faithful Tracers of Turbulent Acceleration

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## EXPERIMENTAL SETUP

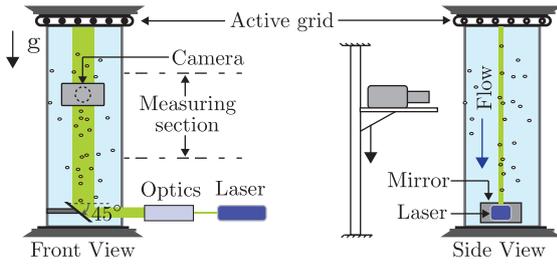


FIG. 1: Schematic of the measurement section of the Twente Water Tunnel. Bubbles and neutrally buoyant tracer particles of diameters  $\approx 150 \pm 25 \mu\text{m}$  and  $\approx 125 \mu\text{m}$ , respectively, were dispersed in the flow for particle tracking experiments.

## PARTICLE EQUATION OF MOTION

The model equation of motion for a small inertial spherical particle advected by a fluid flow field, with velocity  $\mathbf{U}(\mathbf{X}(\mathcal{T}), \mathcal{T})$ , is:

$$\mathcal{V} \rho_p \ddot{\mathbf{X}} = \mathcal{V} \rho_f \frac{D\mathbf{U}}{D\mathcal{T}} + \mathbf{F}_{\text{AM}} + \mathbf{F}_{\text{D}} + \mathbf{F}_{\text{B}} \quad (1)$$

where  $\mathcal{V} = \frac{4}{3}\pi a^3$  is the particle volume, with  $a$  being the particle radius, and  $\rho_f$  and  $\rho_p$  the fluid and particle mass densities, respectively. The forces contributing on the right-hand-side besides the fluid acceleration (which includes the pressure gradient term) are the added mass  $\mathbf{F}_{\text{AM}}$ , the drag force  $\mathbf{F}_{\text{D}}$ , and the buoyancy  $\mathbf{F}_{\text{B}}$  [1–3]:

$$\mathbf{F}_{\text{AM}} = \mathcal{V} \rho_f C_M \left( \frac{D\mathbf{U}}{D\mathcal{T}} - \ddot{\mathbf{X}} \right), \quad (2)$$

$$\mathbf{F}_{\text{D}} = 6 \pi \mu a (\mathbf{U} - \dot{\mathbf{X}}), \quad (3)$$

$$\mathbf{F}_{\text{B}} = \mathcal{V} (\rho_p - \rho_f) g \hat{\mathbf{e}}_z, \quad (4)$$

where  $\mu$  is the dynamic viscosity,  $g$  is the gravity intensity and  $\hat{\mathbf{e}}_z$  is the unit-vector in the direction of gravity. Note that we use the inviscid added mass coefficient for a sphere, i.e  $C_M = 1/2$ . This leads to

$$\ddot{\mathbf{X}} = \frac{3\rho_f}{\rho_f + 2\rho_p} \left( \frac{D\mathbf{U}}{D\mathcal{T}} + \frac{12\nu}{d_p^2} (\mathbf{U} - \dot{\mathbf{X}}) + g \hat{\mathbf{e}}_z \right) - g \hat{\mathbf{e}}_z, \quad (5)$$

where  $\nu \equiv \mu/\rho_f$  is the kinematic viscosity, and  $d_p$  is the particle diameter. Here we neglect lift, history, and finite-size Faxén forces, since these are verified to be small in point-particle limit and when the particle size is smaller than the Kolmogorov length scale  $\eta$  of the flow [4–6].

## FROUDE NUMBER EFFECT

We first consider the effect of changing the ratio of turbulent to gravitational acceleration, i.e  $a_\eta/g$ , which, according to [7], equals the Froude number. Gravity enhances the acceleration in both vertical and horizontal directions (Fig. 2). The vertical acceleration is consistently lower compared to the horizontal, in agreement with our experiments. This is accompanied by a decrease in correlation time (Fig. 3), as also evidenced by our experiments.

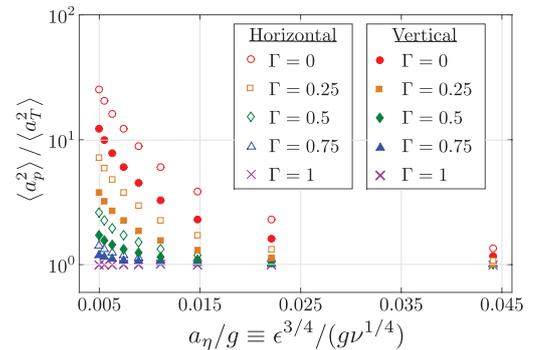


FIG. 2: Normalized acceleration variance for buoyant particles vs  $a_\eta/g$  obtained from Eulerian-Lagrangian DNS at  $\text{Re}_\lambda \approx 80$ . Hollow and solid symbols correspond to horizontal and vertical components, respectively.

## NON-DIMENSIONALIZATION

When the advecting flow is turbulent and the particle spatial extension is of the order of the dissipative scale of turbulence, it is appropriate to non-dimensionalize eq. (5) with respect to the Kolmogorov units:  $\eta$  (length) and  $\tau_\eta$  (time). This leads to

$$\ddot{\mathbf{x}} = \beta \frac{D\mathbf{u}}{Dt} + \frac{1}{St}(\mathbf{u} - \dot{\mathbf{x}}) + \frac{1}{Fr} \hat{\mathbf{e}}_z, \quad (6)$$

where small case letters denote the new dimensionless variables and the following control parameters have been defined:

$$\beta \equiv \frac{3\rho_f}{\rho_f + 2\rho_p}; \quad St \equiv \frac{d_p^2}{12\beta\nu\tau_\eta} = \frac{\tau_p}{\tau_\eta}; \quad Fr \equiv \frac{a_\eta}{(\beta - 1)g} \quad (7)$$

Note that the Stokes number  $St$  is defined taking added mass into account, and the Froude number  $Fr$  is a modified one that takes the particle density, through  $\beta$ , into account. Therefore these definitions are valid for a particle of arbitrary density.

In the high turbulence intensity limit ( $Fr \rightarrow \infty$ ), the third right-hand-side term in the equation of motion can be neglected. Under this condition the vanishing  $St$  limit leads to  $\dot{\mathbf{x}} \simeq \mathbf{u}$  for the velocity, and for the acceleration to  $\ddot{\mathbf{x}} \simeq D_t\mathbf{u}$ , where  $D_t\mathbf{u}$  denotes the fluid-tracer acceleration.

At finite  $Fr$ , the small  $St$  limit leads to  $\dot{\mathbf{x}} \simeq \mathbf{u} + \frac{St}{Fr} \hat{\mathbf{e}}_z$ . For the particle acceleration this implies:

$$\ddot{\mathbf{x}} \simeq D_t\mathbf{u} + \frac{St}{Fr} \partial_z \mathbf{u} \quad (8)$$

## ACCELERATION VARIANCE

We consider the single-component acceleration variance. These are

$$\langle \ddot{x}^2 \rangle \simeq \langle (D_t u_x)^2 \rangle + \left( \frac{St}{Fr} \right)^2 \langle (\partial_z u_x)^2 \rangle, \quad (9)$$

$$(10)$$

where  $x$  and  $z$  are the horizontal and vertical components, respectively. Note that the linear terms in  $St/Fr$  vanish because there is no correlation between terms of the type  $\mathbf{u} \cdot \nabla u_i$  and  $\partial_z u_i$ , i.e. there is no instantaneous correlation between the velocity field and its gradient.

Under isotropic turbulent conditions, the following relations are verified [8]:

$$\langle (\partial_z U_x)^2 \rangle \simeq \frac{2}{15} \frac{\epsilon}{\nu}, \quad (11)$$

$$\langle (\partial_z U_z)^2 \rangle \simeq \frac{1}{15} \frac{\epsilon}{\nu}, \quad (12)$$

$$\langle (D_T U_i)^2 \rangle = a_0 \epsilon^{3/2} \nu^{-1/2}, \quad (13)$$

where  $i$  denotes one of the components  $x$ ,  $y$ , or  $z$ , and  $a_0$  is the so-called Heisenberg-Yaglom constant. From this, one obtains the relations linking the acceleration variance of particles to that of fluid tracers

$$\frac{\langle \ddot{x}^2 \rangle}{\langle (D_t u_x)^2 \rangle} \simeq 1 + \frac{2}{15 a_0} \left( \frac{St}{Fr} \right)^2 \quad (14)$$

$$\frac{\langle \ddot{z}^2 \rangle}{\langle (D_t u_x)^2 \rangle} \simeq 1 + \frac{1}{15 a_0} \left( \frac{St}{Fr} \right)^2 \quad (15)$$

These predictions are applicable to both heavy ( $St/Fr < 1$ ) and light ( $St/Fr > 1$ ) particles of arbitrary density. On the experimental side, we have confirmed the enhancement of acceleration variance using tiny air-bubbles dispersed in our water tunnel facility. For heavy-particles, our predictions remain to be experimentally verified.

## LAGRANGIAN TIME CORRELATION

In Fig. 3(a), we plot the simulation results for the evolution of Lagrangian time-correlation of acceleration with the ratio  $St/Fr$ . The left branch points to heavy particle, and the right one, to light particles. With increasing magnitude of  $St/Fr$ , we observe a decline in the correlation time for both heavy and light particles. Clearly, the drifting of the buoyant or heavy particle through the flow affects the correlation time. We model this by considering the case of a particle drifting through the flow at a speed  $u_r$ . In the absence of particle drift, it is well-known that the decorrelation time is  $\tau_T \sim \tau_\eta$  [9]. Based on the characteristic velocity of a particle in the turbulent flow,  $u_{rms}$ , we estimate the length scale corresponding to this decorrelation time as  $\Lambda \sim u_{rms} \tau_\eta$ . Now, for a buoyant or heavy particle, the time of correlation is reduced due to an extra drift speed. Therefore, the new correlation time may be written as  $\tau_p \approx \tau_T / (1 + u_r/u_{rms})$ . For homogeneous isotropic turbulence the  $u_{rms}$  may be expressed in terms of the  $Re_\lambda$  and the  $u_\eta$ . This leaves us with the expression:  $\tau_p/\tau_T \approx 1/(1 + \sqrt[4]{5/(3Re_\lambda^2)} \frac{St}{Fr})$ . The predictions, shown by the solid black curve, are in reasonable agreement with our numerical observations.

While the model provides reasonable predictions for the decorrelation time, we observe some small deviations from small to moderate  $St/Fr$  values in Fig. 3(a). Below, we provide an explanation for these deviations. From eq. (8), we note that the acceleration of a drifting particle has two contributions: (a)  $D_t\mathbf{u}$  from the fluid tracer acceleration, and (b)  $\frac{St}{Fr} \partial_z \mathbf{u}$  from the velocity-gradients in the flow. In Fig. 3(b)-(e), we show the normalized time correlation of the particle accelerations and the gradient terms along the particle trajectories. For small  $St/Fr$ , the velocity gradient terms ( $\partial_z u_z$  and  $\partial_z u_x$ ) decorrelate slower as compared to the fluid acceleration term (see

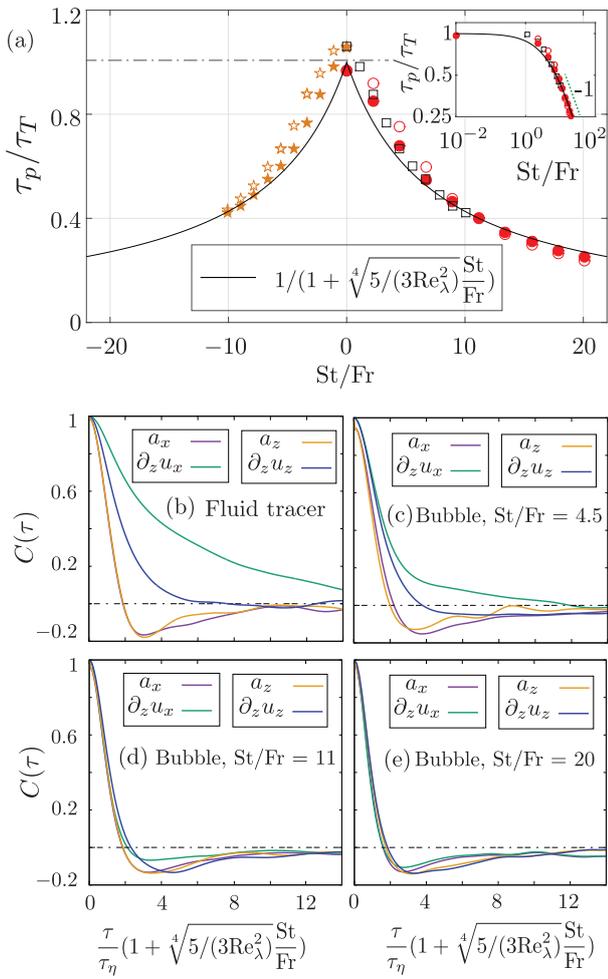


FIG. 3: (a) Normalized correlation time for bubbles ( $\beta = 3$ ) and very heavy ( $\beta = 0$ ) particles vs  $St/Fr$  obtained from Eulerian-Lagrangian DNS at  $Re_\lambda \approx 75$ . The curve in black color shows the theoretical prediction, and the inset shows the plot on log-log scale. (b)-(e) Normalized autocorrelation function for fluid tracers and bubbles at different  $St/Fr$  values. Here,  $a_x$  and  $a_z$  are the horizontal and vertical accelerations, respectively.  $\partial_z u_x$  and  $\partial_z u_z$  are the spatial-velocity gradients, which contribute to the  $a_x$  and  $a_z$ , respectively. In (c)-(e)  $St/Fr$  increases from 4.5 to 20.

Fig. 3(b) & (c)). Since  $St/Fr$  is small, the fluid acceleration term  $D_t \mathbf{u}$  dominates over the velocity gradient term  $\frac{St}{Fr} \partial_z \mathbf{u}$ . This explains the slower decrease in the decorrelation time in the numerics as compared to our predictions for small  $St/Fr$  (see  $|St/Fr| < 5$  in Fig. 3(a)). Some additional observations may be made for the moderate  $St/Fr$  range. From Fig. 3(a), we note that the vertical component of particle acceleration (solid symbols) is shorter-correlated compared to the horizontal component (hollow symbols). This occurs because the fluid velocity gradient components are not all correlated in the same way. Due to the incompressibility constraint ( $\partial_i u_i = 0$ ), the longitudinal gradient  $\partial_z u_z$  is shorter-correlated compared to

the transverse gradient  $\partial_z u_x$ , as may be seen in Fig. 3(b) & (c). Since the vertical acceleration is influenced by the longitudinal velocity-gradient, it decorrelates in shorter time than the horizontal acceleration. We now consider the case of large  $St/Fr$  in Fig. 3(a). In this case, the velocity gradient term  $\frac{St}{Fr} \partial_z \mathbf{u}$  in eq. (8) dominates over the fluid acceleration term  $D_t \mathbf{u}$ , and therefore, the decrease in correlation time in DNS is in good agreement with the predictions of our eddy-crossing model.

## ACCELERATION INTERMITTENCY

Intermittency, i.e. the observed strong deviations from Gaussianity, can be characterized in terms of the flatness of acceleration  $\mathcal{F}(a_p) \equiv \langle a_p^4 \rangle / \langle a_p^2 \rangle^2$ . Assuming statistical independence between  $D_t u_i$  and  $\partial_z u_i$ , we obtain the tracer-normalized flatness of particle acceleration,

$$\frac{\mathcal{F}(\ddot{x})}{\mathcal{F}(D_t u_x)} = \frac{1 + \frac{12}{15 a_0 \mathcal{F}(D_t u_x)} \left(\frac{St}{Fr}\right)^2 \left(1 + \frac{\mathcal{F}(\partial_z u_x)}{45 a_0} \left(\frac{St}{Fr}\right)^2\right)}{1 + 2 \frac{2}{15 a_0} \left(\frac{St}{Fr}\right)^2 + \left(\frac{2}{15 a_0}\right)^2 \left(\frac{St}{Fr}\right)^4} \quad (16)$$

$$\frac{\mathcal{F}(\ddot{z})}{\mathcal{F}(D_t u_x)} = \frac{1 + \frac{6}{15 a_0 \mathcal{F}(D_t u_x)} \left(\frac{St}{Fr}\right)^2 \left(1 + \frac{\mathcal{F}(\partial_z u_z)}{90 a_0} \left(\frac{St}{Fr}\right)^2\right)}{1 + 2 \frac{1}{15 a_0} \left(\frac{St}{Fr}\right)^2 + \left(\frac{1}{15 a_0}\right)^2 \left(\frac{St}{Fr}\right)^4} \quad (17)$$

In the limit of small  $St/Fr$ ,

$$\frac{\mathcal{F}(\ddot{x})}{\mathcal{F}(D_t u_x)} \simeq 1 - \frac{4}{15 a_0} \left(1 - \frac{3}{\mathcal{F}(D_t u_x)}\right) \left(\frac{St}{Fr}\right)^2 \quad (18)$$

$$\frac{\mathcal{F}(\ddot{z})}{\mathcal{F}(D_t u_x)} \simeq 1 - \frac{2}{15 a_0} \left(1 - \frac{3}{\mathcal{F}(D_t u_x)}\right) \left(\frac{St}{Fr}\right)^2 \quad (19)$$

It is verified that  $\mathcal{F}(D_t u_x) > 3$ . Therefore, both components are decreasing functions of  $St/Fr$ , with the vertical being larger than the horizontal one for small  $St/Fr$ .

In the large  $St/Fr$  limit,

$$\frac{\mathcal{F}(\ddot{x})}{\mathcal{F}(D_t u_x)} \simeq \frac{\mathcal{F}(\partial_z u_x)}{\mathcal{F}(D_t u_x)} \quad (20)$$

$$\frac{\mathcal{F}(\ddot{z})}{\mathcal{F}(D_t u_x)} \simeq \frac{\mathcal{F}(\partial_z u_z)}{\mathcal{F}(D_t u_x)} \quad (21)$$

It is verified that  $\mathcal{F}(\partial_z u_z) < \mathcal{F}(\partial_z u_x) < \mathcal{F}(D_t u_x)$  [10]. This leads to the prediction  $\mathcal{F}(a_v) < \mathcal{F}(a_h)$  i.e. vertical acceleration is less intermittent compared to the horizontal.

## INTERPRETATION

Eq. (18)-(19) and eq. (20)-(21) provide predictions for the normalized acceleration flatness (intermittency) in the limits

<sup>1</sup> The absence of correlations between  $D_t u_i$  and  $\partial_z u_i$  is a first order (to be refined) approximation.

of small  $St/Fr$  and large  $St/Fr$ , respectively. Eq. (18)-(19) predict that the vertical component of flatness exceeds the horizontal one in the small  $St/Fr$  limit, while eq. (20)-(21) predict that the horizontal component exceeds the vertical one when  $St/Fr$  is large. Therefore, an interesting cross-over is predicted between the flatness factors of the two components as one moves from small  $St/Fr$  to large  $St/Fr$ . In Fig. 4, we present our numerical results in the small  $St/Fr$  range ( $St/Fr < 1$ ). Despite the scatter in data, we make some interesting observation about our numerical results. With the exception of a single datapoint, the vertical components (solid symbols) are always higher compared to the horizontal components (hollow symbols), in agreement with eq. (18)-(19). In the large  $St/Fr$  limit, as was clear from Figure 4(c) of the main paper, the horizontal component exceeded the vertical one, again in agreement with our predictions (eq. (20)-(21)). Therefore, the cross-over predicted by us is qualitatively seen in our simulations as well. A quantitative agreement is missing since the higher moments (Flatness) are in general very sensitive. Moreover, the lowest Stokes numbers possible in simulations is  $\approx 0.05$ , which is still an approximation of the  $St \rightarrow 0$  limit. In addition, the predictions are subject to a few assumptions, such as the absence of correlation between velocity field and its gradient. While this is reasonable, it is not an exact result. At present, we do not have the resolution to verify the intricate details of (18)-(19). These aspects may be tested in future studies.

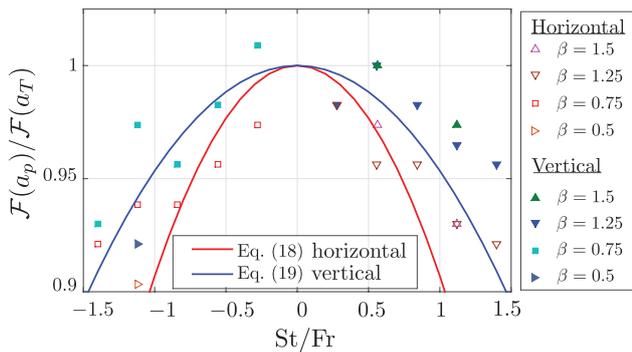


FIG. 4: Normalized Flatness factor in the small  $St/Fr$  limit. Hollow symbols show the flatness fo horizontal acceleration. Solid symbols show the flatness of vertical acceleration. The vertical acceleration flatness is mostly higher in numerics, in qualitative agreement with the predictions of eq. (18)-(19).

## A GENERALIZED APPROACH

We discuss some of these recent analytical and numerical approaches for heavy particles. Interesting effects have been demonstrated on the gravity-induced modification of

heavy particle statistics [7, 11–14], which were quantified as a function of particle inertia ( $St$ ) and the Froude number given by the ratio of turbulent to gravitational acceleration ( $a_\eta/g$ ). We examine the Stokes and Froude number definitions used in these studies. The Stokes number was defined as  $St \equiv \frac{\rho_p d_p^2}{18\rho_f \nu \tau_\eta}$  [7, 12, 14]. This definition is appropriate at large  $\rho_p/\rho_f$ , when added mass effects are negligible. We also note that the definition of Froude number as  $a_\eta/g$  [7, 14] does not take the particle density into account. Here,  $a_\eta$  is the turbulent acceleration and  $g$  is the gravitational acceleration. This Froude number definition is applicable when the particles under consideration are of fixed  $\rho_p/\rho_f$ . Therefore, these results apply to the case of very heavy particles and when the density ratio is kept constant, i.e  $\rho_p/\rho_f = \text{constant} \gg 1$ .

In this paper (main article), we provide a generalized description that is applicable to particles of arbitrary density. We have numerically shown the validity of our theoretical predictions for particles of arbitrary density. The theory we develop for isotropic turbulence can explain also our experimental findings on bubbles in a turbulent water flow. The generic  $St$  and  $Fr$  definitions we use converge to the definitions in [7, 12, 14] at large  $\rho_p/\rho_f$ . Therefore, such a modified approach may be useful for future studies that explore the effects of gravity for arbitrary-density particles in turbulence.

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